A1 conc.

the grating is by elasto-optic or thermo-optic effects. The elasto-optic tuning is usually effected by applying a strain to the grating. Illustratively, this strain results in a Bragg wavelength shift of approximately 1pm/microStrain. Using thermo-optic tuning, the wavelength shift is illustratively approximately 10pm/°C.

2. Please replace paragraph **[0190]** with the following paragraph:

A2

[0190] The thickness uniformity in the linear direction may be controlled by the target configuration and size. To this end, in accordance with an exemplary embodiment of the present invention, sputtered and evaporated materials leave the source (target or crucible) based on a $\cos^n(x)$ law, where x is the distance from the plane of the source. Magnetron sputtering using a planar source and the rate of the material leaving the target is different from position to position depending on the magnetron design. For example, a 15"x15" planar target can cover a uniform deposition region of 12" x 12" (to 5%-10% variation if there is no substrate location). Using such targets uniform coatings on 16 cm non-linearly chirped fiber Bragg gratings illustratively were deposited.

IN THE CLAIMS

1. Please amend Claim 6 as follows:

A3

6. (Amended) A method as recited in claim 5, wherein said adhesion layer is chosen from the group consisting essentially of: Cr, Cr_2O_3, Al_2O_3, Ti, and Si_3N_4.

2. Please amend Claim 18 as follows:

A4

18. (Amended) An optical element as recited in claim 17, wherein said adhesion layer is chosen from the group consisting essentially of: Cr, Cr_2O_3, Al_2O_3, Ti, and Si_3N_4.